

Finite Volume Method for Convection Derivatives II

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Mechanical Engineering 692
Computational Fluid Dynamics

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Outline

- Review finite-volume convection
 - Note need for average ϕ value at cell faces for convection terms
 - Examine use of arithmetic mean as average value and show its problems
- Look at other schemes
 - Upwind differencing
 - Hybrid and power law
 - Total variation diminishing (TVD)

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Review Convection Terms

- Steady equation with convection and diffusion terms in one dimension $\frac{d\rho u \phi}{dx} = \frac{d}{dx} \Gamma \frac{d\phi}{dx}$
- Steady continuity equation in one dimension $\frac{d\rho u}{dx} = 0$
- Apply finite volume approach to integrate small volume

$$\int \frac{d\rho u \phi}{dx} dV = \int \frac{d}{dx} \Gamma \frac{d\phi}{dx} dV \quad \int \frac{d\rho u}{dx} dV = 0$$

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Review Integrated PDE

- Constant area result
 - Define $F = \rho u$ and $D = \Gamma/\delta x$
- Use (second-order accurate) arithmetic mean for face values

$$F_e \phi_e - F_w \phi_w = D_e (\phi_E - \phi_P) - D_w (\phi_P - \phi_W)$$

$$F_e \frac{\phi_E + \phi_P}{2} - F_w \frac{\phi_P + \phi_W}{2} = D_e (\phi_E - \phi_P) - D_w (\phi_P - \phi_W)$$

$$a_E = D_e + \frac{F_e}{2} \quad a_W = D_w + \frac{F_w}{2} \quad a_P = a_E + a_W + F_e - F_w$$

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$$a_W \phi_W - a_P \phi_P + a_E \phi_E = 0$$

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Review Example Problem

- Constant ρ , u , and Γ with $\phi = \phi_0$ at $x = 0$ and $\phi = \phi_L$ at $x = L$
- Exact solution below with plot on next slide

$$\frac{\phi(x) - \phi_0}{\phi_L - \phi_0} = \frac{e^{\frac{\rho u x}{\Gamma}} - 1}{e^{\frac{\rho u L}{\Gamma}} - 1}$$

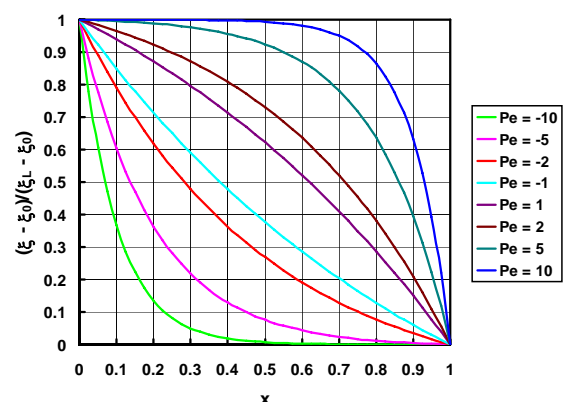
$$Pe = \rho u L / \Gamma$$

$$Pe_{\text{cell}} = \rho u \delta x / \Gamma = F/D$$

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Exact Solution

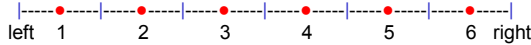


Review Numerical Solution

- Here δx , ρu and Γ are constants

$$-F_e = F_w = \rho u = F \quad D_e = D_w = \Gamma / \delta x = D$$

$$a_W \phi_W - a_P \phi_P + a_E \phi_E = \left(F + \frac{D}{2}\right) \phi_W - 2F \phi_P + \left(F - \frac{D}{2}\right) \phi_E = 0$$



- Boundary conditions at $x = 0$ and $x = L$

$$-\left(\frac{F}{2} + 3D\right) \phi_1 + \left(D - \frac{F}{2}\right) \phi_2 = -(F + 2D) \phi_{left}$$

$$\left(D + \frac{F}{2}\right) \phi_{N-2} - \left(3D - \frac{F}{2}\right) \phi_{N-1} = -(2D - F) \phi_{right}$$

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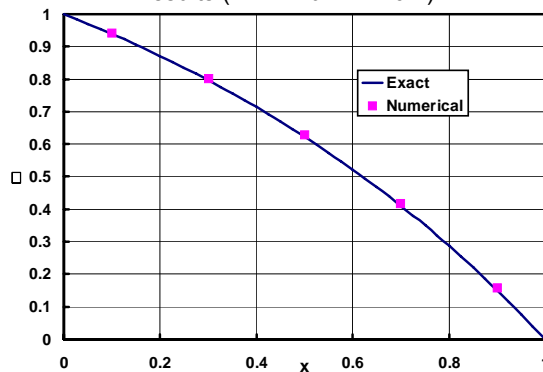
Review Numerical Solution II

- Data: $L = 1$ m, $u = 0.1$ m/s, $\Gamma = 0.1$ kg/m \cdot s, $\delta x = 0.2$ m, $\rho = 1$ kg/m 3
 - $F = \rho u = (1 \text{ kg/m}^3)(0.1 \text{ m/s}) = 0.1 \text{ kg/m}^2\cdot\text{s}$
 - $D = \Gamma / \delta x = (0.1 \text{ kg/m}\cdot\text{s})(0.2 \text{ m}) = 0.5 \text{ kg/m}^2\cdot\text{s}$
 - Ratio $F/D = 0.2$
- Second case: change from 0.1 m/s to 2.5 m/s changing F/D from 0.2 to 5
- Third case: leave u at 0.1 m/s; change δx from 0.2 to 0.05 changing F/D to 1.25

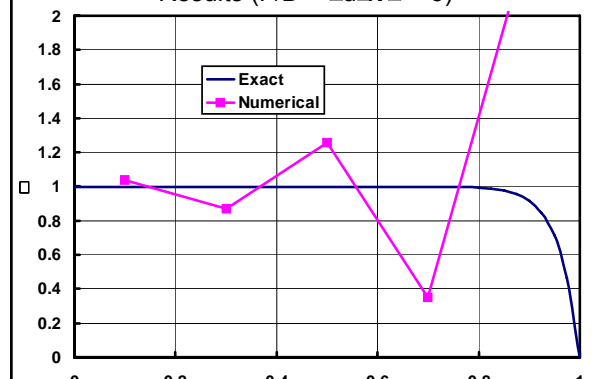
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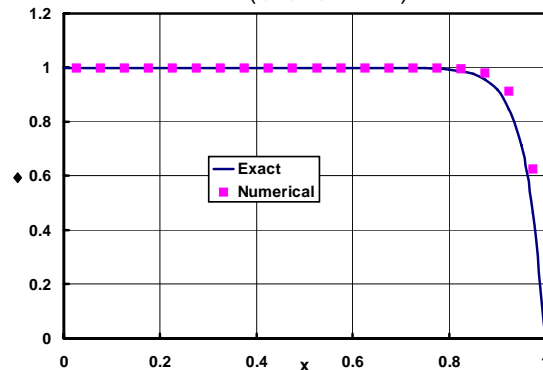
Comparison of Numerical and Exact Results ($F/D = \square u \delta x / \square = 0.2$)



Comparison of Numerical and Exact Results ($F/D = \square u \delta x / \square = 5$)



Comparison of Numerical and Exact Results ($\diamond u \delta x / \diamond = 1.25$)



What is Happening Here?

- When flow term $F = \rho u$ is large compared to diffusion term $D = \delta x / \Gamma$ the use of average values does not recognize the directionality of the flow
- Keeping the F/D ratio small allows use of average values in convection terms
 - Requires small δx for large flow rates
- How can we use larger δx for large flow rates and keep accuracy?

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Algorithm Properties

- Conservative schemes – conserve properties in finite difference equations
 - Requires exit flux from one face to be same as input flux in adjacent cell
- Transportive schemes – have correct balance between diffusion and convection
- Accuracy – need schemes that have a good truncation error

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Algorithm Properties II

- Limit on coefficient magnitude for iteration schemes (boundedness)
 - Absolute value of diagonal coefficient must be greater than the sum of absolute values of all other coefficients
 - For simple equations here $|a_P| \geq |a_E| + |a_W|$
 - Deferred correction separates coefficients into two parts
 - Adjustment leaves $|a_P| \geq |a_E| + |a_W|$
 - Places part removed from adjusted coefficients into source term

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Upwind Convection Term

- Models directionality of flow
- Previously we replaced $F_e \phi_e$ by $F_e(\phi_E + \phi_P)/2$ in convection term
- Upwind difference uses $\phi_e = \phi_P$ if F_e is positive and $\phi_e = \phi_E$ if F_e is negative
- Start with basic finite volume equation

$$F_e \phi_e - F_w \phi_w = D_e(\phi_E - \phi_P) - D_w(\phi_P - \phi_W)$$

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Positive F Terms

- If F_e and F_w are both positive then $\phi_e = \phi_P$ and $\phi_w = \phi_W$

$$\begin{aligned} F_e \phi_e - F_w \phi_w &= D_e(\phi_E - \phi_P) - D_w(\phi_P - \phi_W) \\ F_e \phi_P - F_w \phi_W &= D_e(\phi_E - \phi_P) - D_w(\phi_P - \phi_W) \\ 0 &= D_e \phi_E - (D_e + F_e + D_w) \phi_P + (D_w + F_w) \phi_W \\ a_P &= D_e + F_e + D_w + F_w - F_w = D_e + D_w + F_w + F_e - F_w \\ a_E &= D_e \quad a_W = D_w + F_w \quad a_P = a_E + a_W + F_e - F_w \end{aligned}$$

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Negative F Terms

- If F_e and F_w are both negative then $\phi_e = \phi_E$ and $\phi_w = \phi_P$

$$\begin{aligned} F_e \phi_e - F_w \phi_w &= D_e(\phi_E - \phi_P) - D_w(\phi_P - \phi_W) \\ F_e \phi_E - F_w \phi_P &= D_e(\phi_E - \phi_P) - D_w(\phi_P - \phi_W) \\ 0 &= (D_e - F_e) \phi_E - (D_e - F_w + D_w) \phi_P + D_w \phi_W \\ a_P &= D_e - F_w + D_w + F_e - F_e = D_e - F_e + D_w + F_e - F_w \\ a_E &= D_e - F_e \quad a_W = D_w \quad a_P = a_E + a_W + F_e - F_w \end{aligned}$$

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Computational Formulas

- Positive F terms

$$a_E = D_e \quad a_W = D_w + F_w \quad a_P = a_E + a_W + F_e - F_w$$

- Negative F terms

$$a_E = D_e - F_e \quad a_W = D_w \quad a_P = a_E + a_W + F_e - F_w$$

- Computational formulas

$$a_W = D_w + \max(F_w, 0) \quad a_E = D_e + \max(-F_e, 0)$$

$$a_P = a_E + a_W + F_e - F_w$$

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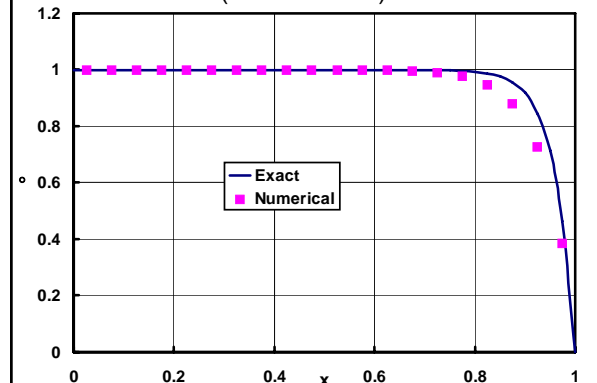
Upwind Solution

- Case III for previous problem
 - $L = 1$ m
 - $u = 0.1$ m/s
 - $\Gamma = 0.1$ kg/m·s
 - $\delta x = 0.05$ m
 - $\rho = 1$ kg/m³
- $F = \rho u = (1 \text{ kg/m}^3)(2.5 \text{ m/s}) = 2.5 \text{ kg/m}^2\cdot\text{s}$
- $D = \Gamma/\delta x = (0.1 \text{ kg/m}\cdot\text{s}) / (0.05 \text{ m}) = 2 \text{ kg/m}^2\cdot\text{s}$
- Ratio $F/D = 1.25 = \text{Pe}_{\text{cell}}$

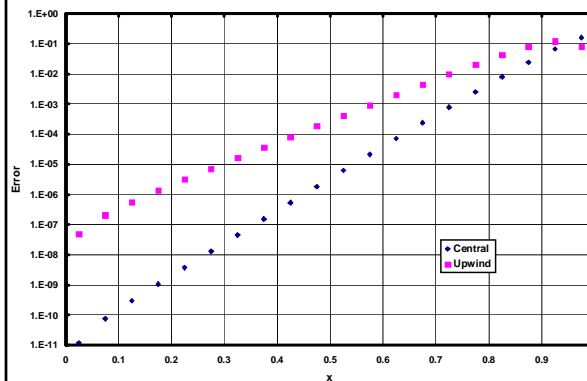
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Comparison of Upwind and Exact Results ($\phi u \phi / \phi = 1.25$)



Errors in CFD Algorithms for Model Problem with $\text{Pe}_{\text{cell}} = 1.25$



Other Algorithms

- Hybrid algorithm
 - Combination of central difference for $\text{Pe}_{\text{cell}} < 2$ and upwind for $\text{Pe}_{\text{cell}} \geq 2$

$$a_W = \max \left[F_w, \left(D_w + \frac{F_w}{2} \right), 0 \right] \quad a_E = \max \left[-F_e, \left(D_e + \frac{F_e}{2} \right), 0 \right]$$

$$a_P = a_E + a_W + F_e - F_w$$

- Power-law algorithm
 - Similar to hybrid
 - Sets $D = 0$ for $|\text{Pe}_{\text{cell}}| > 10$
 - Uses power law formula for $|\text{Pe}_{\text{cell}}| \leq 10$

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Other Algorithms II

– Power law formula $a_P = a_E + a_W + F_e - F_w$

$$a_W = D_w \max \left[0, \left(1 - |Pe_w|^5 \right) \right] + \max [F_w, 0] \quad Pe_w = F_w / D_w$$

$$a_E = D_e \max \left[0, \left(1 - |Pe_e|^5 \right) \right] + \max [-F_e, 0] \quad Pe_e = F_e / D_e$$

- QUICK – Quadratic Upstream Interpolation for Convective Kinetics
 - Uses quadratic interpolation formula
 - Choose nodes to use for interpolation depending on velocity

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Other Algorithms III

- QUICK formulas for central node P involve five nodes instead of three

WW ww W w P e E ee EE

$$a_{WW}\phi_{WW} + a_W\phi_W - a_P\phi_P + a_E\phi_E + a_{EE}\phi_{EE} = 0$$

$$a_W = D_w + \frac{6\alpha_w F_w + 3(1-\alpha_w)F_w + \alpha_e F_e}{8} \quad a_{WW} = -\frac{\alpha_w F_w}{8}$$

$$a_E = D_e - \frac{3\alpha_e F_e + 6(1-\alpha_e)F_e + (1-\alpha_w)F_w}{8} \quad a_{EE} = \frac{(1-\alpha_e)F_e}{8}$$

$$\alpha_w = 1 \text{ if } F_w > 0 \text{ and } \alpha_e = 1 \text{ if } F_e > 0$$

$$\alpha_w = 0 \text{ if } F_w < 0 \text{ and } \alpha_e = 0 \text{ if } F_e < 0$$

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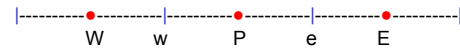
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Homework for March 3

- Download the Excel workbook from the course web site for the sample convection problem with $Pe_{cell} = 1.25$
 - Shows results for Central and Upwind on separate worksheets
- Add similar worksheets to get results for Hybrid, Power Law, and QUICK
- Add error results for these algorithms to the error chart

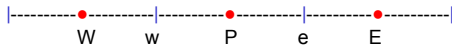
TVD Algorithms

- Total Variation Diminishing** schemes
 - Designed to maintain both accuracy and stability with no unphysical "wiggles"
 - Consider set of different differencing schemes for ϕ_e with positive u velocity



- Upwind: $\phi_e = \phi_P$
- Linear Upwind: $\phi_e = \phi_P + \frac{\phi_P - \phi_W}{x_P - x_W}(x_e - x_P)$
 - For constant δx : $\phi_e = \phi_P + \frac{\phi_P - \phi_W}{2}$

TVD Algorithms II



- QUICK: $\phi_e = \phi_P + \frac{3\phi_E - 2\phi_P - \phi_W}{8}$
- Second order: $\phi_e = \phi_P + \frac{\phi_E - \phi_P}{2}$
- General form is $\phi_e = \phi_P + \text{Correction}$
- Correction can always be written as a correction $(\psi/2)$ times $\phi_E - \phi_P$
- Correction function ψ depends on $(\phi_P - \phi_W)/(\phi_E - \phi_P)$

Why TVD?

- Developed for transient compressible gas dynamics equations
- Scheme to obtain accurate compromise between false diffusion of upwinding and "wiggles" of more accurate schemes in some regions
- Basic development mathematically complex, but results useful
- Basic equation $\phi_e = \phi_P + \psi(r)(\phi_E - \phi_P)/2$
 - $r = (\phi_P - \phi_W)/(\phi_E - \phi_P)$

What is ψ ?

- Upwind: $\phi_e = \phi_P$ $\psi = 0$
- Second order arithmetic mean:

$$\phi_e = \phi_P + \frac{\phi_E - \phi_P}{2} = \frac{1}{2}(\phi_E - \phi_P) \Rightarrow \psi = 1$$

- Linear upwind with constant δx :

$$\phi_e = \phi_P + \frac{\phi_P - \phi_W}{2} = \phi_P + \frac{1}{2} \frac{\phi_P - \phi_W}{\phi_E - \phi_P} (\phi_E - \phi_P) = \phi_P + \frac{1}{2} r (\phi_E - \phi_P) \Rightarrow \psi = r$$

- QUICK (after some algebra)

$$\phi_e = \phi_P + \frac{1}{2} \left[\frac{1}{4} \left(3 + \frac{\phi_P - \phi_W}{\phi_E - \phi_P} \right) \right] (\phi_E - \phi_P) = \phi_P + \frac{1}{2} \left[\frac{3+r}{4} \right] (\phi_E - \phi_P) \Rightarrow \psi = \frac{3+r}{4}$$

TVD Region Limits on $\psi(r)$

- For $0 < r \leq 1$, $\psi(r) \leq 2r$
- For $r \geq 1$, $\psi(r) \leq 2$
- For second-order accuracy and TVD
 - For $0 < r \leq 1$, $r \leq \psi(r) \leq 2r$
 - For $1 \geq r \geq 2$, $1 \leq \psi(r) \leq r$
 - For $r > 2$, $1 \leq \psi(r) \leq 2$
- Implementation of TVD requires parts of coefficient terms in S_u term as deferred correction

