

Numerical Heat Transfer

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Mechanical Engineering 375
Heat Transfer

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Outline

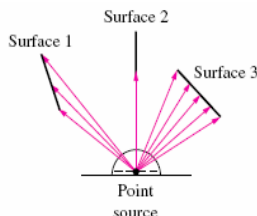
- What is numerical analysis
- Considerations of conduction, convection and radiation
- Review numerical analysis basics
 - Derivative expressions, truncation error and roundoff error
- Numerical solutions of the conduction equation in one space dimension
- Explicit versus implicit algorithms



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Review View Factor, $F_{i \rightarrow j}$ or F_{ij}

- $F_{i \rightarrow j}$ or F_{ij} is the fraction of radiation, leaving surface i , that strikes surface j
 - $A_i F_{ij} = A_j F_{ji}$
 - $\sum_j F_{ij} = 1$
 - $F_{1 \rightarrow 2+3} = F_{1 \rightarrow 2} + F_{1 \rightarrow 3}$



- Find view factors from charts or equations
- Basic component of radiation exchange



Figure 13-1 from Çengel, Heat and Mass Transfer

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Review All Black Surfaces

- Heat transfer from surface 1 reaching surface 2 is $A_1 F_{12} \sigma T_1^4$
- Heat transfer from surface 2 reaching surface 1 is $A_2 F_{21} \sigma T_2^4 = A_1 F_{12} \sigma T_2^4$
- Net heat transfer from surface 1 is $A_1 F_{12} \sigma (T_1^4 - T_2^4)$
 - Negative value indicates heat into surface 1
 - For multiple surfaces

$$\dot{Q}_i = \sum_{j=1}^N \dot{Q}_{i \rightarrow j} = \sum_{j=1}^N A_i F_{ij} \sigma (T_i^4 - T_j^4)$$



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Review Gray Diffuse Opaque

- Kirchoff's law applies to the average: $\alpha = \varepsilon$ at all temperatures
- For opaque surfaces $\tau = 0$ so $\alpha + \rho = 1$
- For gray, diffusive, opaque surfaces then $\rho = 1 - \alpha = 1 - \varepsilon$
- Define radiosity, $J = \varepsilon E_b + \rho G =$ emitted and reflected radiation

$$\dot{Q}_i = \frac{A_i \varepsilon_i (E_{bi} - J_i)}{1 - \varepsilon_i} = \frac{E_{bi} - J_i}{R_i} \quad \text{where} \quad R_i = \frac{1 - \varepsilon_i}{A_i \varepsilon_i}$$



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Review Gray Diffuse Opaque II

$$\dot{Q}_i = \sum_{j=1}^N \dot{Q}_{ij} = \sum_{j=1}^N A_i F_{ij} (J_i - J_j) = \sum_{j=1}^N \frac{J_i - J_j}{R_{ij}} \quad R_{ij} = \frac{1}{A_i F_{ij}}$$

- Combining two equations for $\dot{Q}_i$

$$\sum_{j=1}^N \frac{J_i - J_j}{R_{ij}} = \frac{E_{bi} - J_i}{R_i} \Rightarrow \sum_{j=1}^N \frac{J_i - J_j}{R_{ij}} + \frac{J_i - E_{bi}}{R_i} = 0$$

- Solve system of N simultaneous linear equations for N values of J_i
- Black or reradiating surface ($\dot{Q}_i = 0$) has $J_i = E_{bi} = \sigma T_i^4$

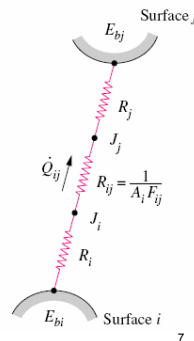


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Review Circuit Analogy

- Look at simple enclosure with only two surfaces
- Apply circuit analog with total resistance

$$\dot{Q}_{12} = \frac{E_{b1} - E_{b2}}{R_{Total}} = \frac{E_{b1} - E_{b2}}{\frac{1 - \epsilon_1}{A_1 F_{11}} + \frac{1}{A_1 F_{12}} + \frac{1 - \epsilon_2}{A_2 F_{22}}}$$



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Review Three-Surface Circuit

- If $\dot{Q}_3 = 0$, $\dot{Q}_{net,1 \rightarrow 2}$ can be found from circuit with two parallel resistances

$$\dot{Q}_{net,12} = \frac{E_{b1} - E_{b2}}{R_{Total}} = \frac{E_{b1} - E_{b2}}{R_1 + R_{\downarrow} + R_2} \quad R_{\downarrow} = \frac{1}{\frac{1}{R_{12}} + \frac{1}{R_{13} + R_{23}}}$$

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Review Radiation Exchange

- Two possible surface conditions: (1) known temperature, (2) known $\dot{Q}_i$

$$\dot{Q}_i = \frac{A_i \epsilon_i}{1 - \epsilon_i} (E_{bi} - J_i) = \sum_{j=1}^N A_i F_{ij} (J_i - J_j) \quad i = 1, \dots, N$$

$$(1) \left(1 + \frac{1 - \epsilon_i}{\epsilon_i} \sum_{j=1, j \neq i}^N F_{ij} \right) J_i - \frac{1 - \epsilon_i}{\epsilon_i} \sum_{j=1, j \neq i}^N F_{ij} J_j = E_{bi} = \sigma T_i^4$$

$$(2) \left(\sum_{j=1, j \neq i}^N A_i F_{ij} \right) J_i - \sum_{j=1, j \neq i}^N A_i F_{ij} J_j = \dot{Q}_i$$

Solve this set of N simultaneous equations for N values of J_i

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Review Radiation Exchange II

- Once all J_i values are known we can compute unknown values of T_i and $\dot{Q}_i$
 - For known T_i

$$\dot{Q}_i = \frac{A_i \epsilon_i}{1 - \epsilon_i} (E_{bi} - J_i) = \frac{A_i \epsilon_i}{1 - \epsilon_i} (\sigma T_i^4 - J_i)$$

- For known $\dot{Q}_i$

$$E_{bi} = J_i + \frac{1 - \epsilon_i}{A_i \epsilon_i} \dot{Q}_i \Rightarrow T_i = \frac{1}{\sigma} \sqrt[4]{J_i + \frac{1 - \epsilon_i}{A_i \epsilon_i} \dot{Q}_i}$$

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Numerical Analysis

- Differential equations give analytical solution at any point
- Usually not possible to obtain analytical solutions for real problems
- Numerical analysis provides algebraic equations for values at a set of points in region
 - Larger sets give better values of temperature and temperature gradient required for heat transfer

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Numerical Analysis II

- Use different methods
 - Finite differences use Taylor series to get pointwise expressions for differential equations with measure of error
 - Finite element methods use integral approach to get similar results
 - Finite volume methods are midway between the two
 - Can use physical arguments to derive algebraic equations (see text)

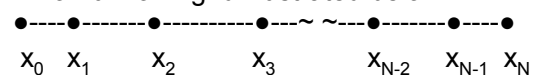
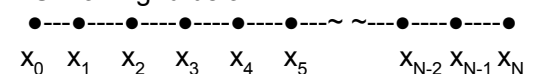
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Finite Difference Grids

- Subdivide region into discrete points
- Spacing between the points may be uniform or non-uniform
- Example: grid for $x_{\min} \leq x \leq x_{\max}$ with $N+1$ nodes numbered from zero to N
- Initial node value, $x_0 = x_{\min}$
- Final grid node value, $x_N = x_{\max}$
- Node spacing between $\Delta x_i = x_i$ and x_{i-1}
- Uniform spacing, $h = \Delta x_i = (x_{\max} - x_{\min})/N$
- $N+1$ nodes give N spaces

Finite Difference Grids II

- Non-uniform grid illustrated below
- 
- Uniform grid below
- 
- Can have two, three or four-dimensional grids for x , y , z , and time
 - Notation $T_{ijk}^n = T(x_i, y_j, z_k, t_n)$

Derivative Expressions

- Obtain from differentiating interpolation polynomials or from Taylor series
- Manipulate equation to get expression for derivative plus error term

$$f(x) = f(a) + \frac{df}{dx}\bigg|_{x=a} (x-a) + \frac{1}{2!} \frac{d^2 f}{dx^2}\bigg|_{x=a} (x-a)^2 + \frac{1}{3!} \frac{d^3 f}{dx^3}\bigg|_{x=a} (x-a)^3 + \dots$$

- Apply to $a = x_i$ and $x = x_{i+1}$

$$f(x_{i+1}) = f(x_i) + \frac{df}{dx}\bigg|_{x=x_i} (x_{i+1} - x_i) + \frac{1}{2!} \frac{d^2 f}{dx^2}\bigg|_{x=x_i} (x_{i+1} - x_i)^2 + \frac{1}{3!} \frac{d^3 f}{dx^3}\bigg|_{x=x_i} (x_{i+1} - x_i)^3 + \dots$$

$$\frac{df}{dx}\bigg|_{x=x_i} = \frac{f(x_{i+1}) - f(x_i)}{x_{i+1} - x_i} + \frac{1}{2!} \frac{d^2 f}{dx^2}\bigg|_{x=x_i} (x_{i+1} - x_i) + \frac{1}{3!} \frac{d^3 f}{dx^3}\bigg|_{x=x_i} (x_{i+1} - x_i)^2 + \dots$$

Derivative Expressions II

- Look at the first term in the error
- Can show that this equals error if location if derivative is unknown

$$\frac{df}{dx}\bigg|_{x=x_i} = \frac{f(x_{i+1}) - f(x_i)}{x_{i+1} - x_i} + \frac{1}{2!} \frac{d^2 f}{dx^2}\bigg|_{x=x_i} \frac{(x_{i+1} - x_i)^2}{x_{i+1} - x_i} + \frac{1}{3!} \frac{d^3 f}{dx^3}\bigg|_{x=x_i} \frac{(x_{i+1} - x_i)^3}{x_{i+1} - x_i} + \dots$$

$$\frac{df}{dx}\bigg|_{x=x_i} = \frac{f(x_{i+1}) - f(x_i)}{x_{i+1} - x_i} + \frac{1}{2!} \frac{d^2 f}{dx^2}\bigg|_{x=\xi} \frac{(x_{i+1} - x_i)^2}{x_{i+1} - x_i}$$

- For uniform $x_{i+1} - x_i = \Delta x = h$

$$\frac{df}{dx}\bigg|_{x=x_i} = \frac{f(x_{i+1}) - f(x_i)}{h} + \frac{1}{2!} \frac{d^2 f}{dx^2}\bigg|_{x=\xi} h = \frac{f(x_{i+1}) - f(x_i)}{h} + O(h)$$

$O(h)$ is Order of the Error

$$\frac{df}{dx}\bigg|_{x=x_i} = \frac{f(x_{i+1}) - f(x_i)}{h} + O(h) \quad \text{or} \quad \frac{df}{dx}\bigg|_i = f'_i = \frac{f_{i+1} - f_i}{h} + O(h)$$

- Notation $O(h^n)$ means **truncation error** is proportional to h^n
- Error proportional to h^n called n^{th} order
- Changing step size from h_1 to h_2 changes n^{th} order error power of n

$$\varepsilon_2 \approx \varepsilon_1 \left(\frac{h_2}{h_1} \right)^n$$

First Derivative Expressions

$$\text{First order forward} \quad f'_i = \frac{f_{i+1} - f_i}{h} + O(h) \quad \text{First order backward} \quad f'_i = \frac{f_i - f_{i-1}}{h} + O(h)$$

$$\text{Second order central} \quad f'_i = \frac{f_{i+1} - f_{i-1}}{2h} + O(h^2)$$

$$\text{Second order forward} \quad f'_i = \frac{-f_{i+2} + 4f_{i+1} - 3f_i}{2h} + O(h^2)$$

$$\text{Second order backwards} \quad f'_i = \frac{f_{i-2} - 4f_{i-1} + 3f_i}{2h} + O(h^2)$$

Second Derivatives

- Second-order, central-difference, second derivative

$$f''_i = \frac{f_{i+1} + f_{i-1} - 2f_i}{h^2} + O(h^2)$$

- Other expressions available, but this is most common

Find f' and f'' for sin at x = 1

Second order central

$$f'_i = \frac{f_{i+1} - f_{i-1}}{2h} + O(h^2) \qquad f''_i = \frac{f_{i+1} + f_{i-1} - 2f_i}{h^2} + O(h^2)$$

$$f'_i = \frac{\sin(1+.1) - \sin(1-.1)}{2(.1)} \qquad f''_i = \frac{\sin(1+.1) + \sin(1-.1) - 2\sin(1)}{(.1)^2}$$

$$f'_i = \frac{\sin(1+.01) - \sin(1-.01)}{2(.01)} \qquad f''_i = \frac{\sin(1+.01) + \sin(1-.01) - 2\sin(1)}{(.01)^2}$$

$$f'_i = \frac{\sin(1+.001) - \sin(1-.001)}{2(.001)} \qquad f''_i = \frac{\sin(1+.001) + \sin(1-.001) - 2\sin(1)}{(.001)^2}$$

Roundoff Error

- Possible in derivative expressions from subtracting close differences
- Example $f(x) = e^x$: $f'(x) \approx (e^{x+h} - e^{x-h})/(2h)$ and error at $x = 1$ is $(e^{1+h} - e^{1-h})/(2h) - e$

$$E = \frac{3.004166 - 2.722815}{2(.1)} - 2.718282 = 4.5 \times 10^{-3}$$

$$E = \frac{2.718536702 - 2.7180100139}{2(.0001)} - 2.718281828459 = 4.5 \times 10^{-9}$$

$$E = \frac{2.71828210028724 - 2.71828155660388}{2(.00000001)} - 2.718281828 = 5.9 \times 10^{-9}$$

Error vs. Step Size Log Plots

- Previously said that $\epsilon_2 \approx \epsilon_1 \left(\frac{h_2}{h_1} \right)^n$

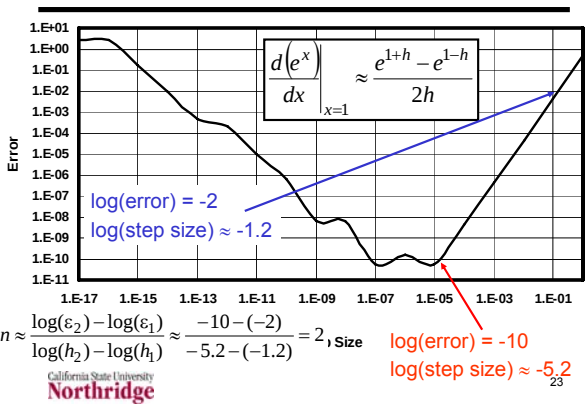
$$\log(\epsilon_2) \approx \log(\epsilon_1) + n \log\left(\frac{h_2}{h_1}\right) = \log(\epsilon_1) + n[\log(h_2) - \log(h_1)]$$

$$\log(\epsilon_2) - \log(\epsilon_1) \approx n[\log(h_2) - \log(h_1)]$$

$$n \approx \frac{\log(\epsilon_2) - \log(\epsilon_1)}{\log(h_2) - \log(h_1)}$$

- The slope of a line on a log(error) vs. log(step size) plot is order of the error

Figure 2-1. Effect of Step Size on Error



Numerical PDE Solutions

- Define a finite-difference grid in the independent variables (x, y, z, t)
- Place grid points on region boundary whose values are found from boundary conditions for the problem
- At some grid location convert differential equation into a finite difference equation
 - Observe truncation error in process
 - Neglect truncation error to get set of algebraic equations to solve

Unsteady Heat Transfer

- Apply difference formulas derived for ordinary derivatives to partial derivatives
- Use notation to consider different coordinate directions $\left[\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial x^2}\right]_i$
- Apply to diffusion equation
- Grids $x_i = x_0 + i\Delta x$ and $t_n = t_0 + n\Delta t$
- Try finite difference expressions below to get simple finite-difference equation

$$\frac{\partial T}{\partial t}_i^n = \frac{T_i^{n+1} - T_i^n}{\Delta t} + O(\Delta t) \quad \text{and} \quad \frac{\partial^2 T}{\partial x^2}_i^n = \frac{T_{i+1}^n + T_{i-1}^n - 2T_i^n}{(\Delta x)^2} + O[(\Delta x)^2]$$

Unsteady Heat Transfer II

- Substitute finite difference expressions into differential equation

$$\frac{T_i^{n+1} - T_i^n}{\Delta t} = \alpha \frac{T_{i+1}^n + T_{i-1}^n - 2T_i^n}{(\Delta x)^2} + O[\Delta t, (\Delta x)^2]$$

- Ignore truncation error, solve for T_i^{n+1}

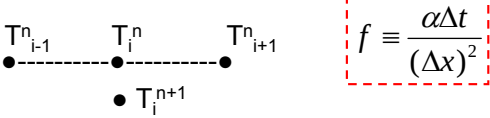
$$T_i^{n+1} = \frac{\alpha \Delta t}{(\Delta x)^2} (T_{i+1}^n + T_{i-1}^n) + \left(1 - \frac{2\alpha \Delta t}{(\Delta x)^2}\right) T_i^n$$

- Obtain temperature at $x = x_i$ and $t = t_{n+1}$ in terms of T values at old time step

Explicit (FTCS) Method

- Method just derived is called explicit method; can solve one equation at a time

$$T_i^{n+1} = \frac{\alpha \Delta t}{(\Delta x)^2} (T_{i+1}^n + T_{i-1}^n) + \left(1 - \frac{2\alpha \Delta t}{(\Delta x)^2}\right) T_i^n = f(T_{i+1}^n + T_{i-1}^n) + (1 - 2f)T_i^n$$



- T_i^{n+1} does not depend on other T values at the new time step (n+1)

Explicit Method Example

- Pick $\alpha = 1$, $\Delta x = 0.25$, $N_x = 4$, $\Delta t = 0.01$
- $f = \alpha \Delta t / (\Delta x)^2 = 1(0.01) / (0.25)^2 = 0.16$
- Pick initial $T_i^0 = 1000$ and boundaries, $T_0^n = T_4^n = 0$ for time > 0 ($n \geq 0$)

$$\text{Apply } T_i^{n+1} = f(T_{i+1}^n + T_{i-1}^n) + (1 - 2f)T_i^n$$

$$T_1^1 = f[T_0^0 + T_2^0] + (1 - 2f)T_1^0 = 0.16[0 + 1000] + 0.68[1000] = 840$$
$$T_2^1 = f[T_1^0 + T_3^0] + (1 - 2f)T_2^0 = 0.16[1000 + 1000] + 0.68[1000] = 1000$$
$$T_3^1 = f[T_2^0 + T_4^0] + (1 - 2f)T_3^0 = 0.16[1000 + 0] + 0.68[1000] = 840$$

- Repeat for subsequent time steps

Explicit Method Results $f = 0.16$

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0.00	x = 0.25	x = 0.50	x = 0.75	x = 1.00
	t = 0	1000	1000	1000	1000	1000
n = 0	t = 0+	0	1000	1000	1000	0
n = 1	t = 0.01	0	840	1000	840	0
n = 2	t = 0.02	0	731.2	948.8	731.2	0
n = 3	t = 0.03	0	649	879.2	649	0
n = 4	t = 0.04	0	582	805.5	582	0
n = 5	t = 0.05	0	524.6	734	524.6	0
n = 6	t = 0.06	0	474.2	667	474.2	0
n = 7	t = 0.07	0	429.2	605.3	429.2	0
n = 8	t = 0.08	0	388.7	548.9	388.7	0

Explicit Method Results $f = 0.16$

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0.00	x = 0.25	x = 0.50	x = 0.75	x = 1.00
n = 12	t = 0.12	0	262	370.5	262	0
n = 13	t = 0.13	0	237.5	335.8	237.5	0
n = 14	t = 0.14	0	215.2	304.4	215.2	0
n = 15	t = 0.15	0	195	275.8	195	0
n = 16	t = 0.16	0	176.8	250	176.8	0
n = 17	t = 0.17	0	160.2	226.5	160.2	0
n = 18	t = 0.18	0	145.2	205.3	145.2	0
n = 19	t = 0.19	0	131.6	186.1	131.6	0
n = 20	t = 0.20	0	119.2	168.6	119.2	0
Exact	t = 0.20	0	125.1	176.9	125.1	0
Error	t = 0.20	0	5.8	8.2	5.8	0

Explicit Results $f = 0.32$

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0.00	x = 0.25	x = 0.50	x = 0.75	x = 1.00
	t = 0	1000	1000	1000	1000	1000
n = 0	t = 0+	0	1000	1000	1000	0
n = 1	t = 0.02	0	680	1000	680	0
n = 2	t = 0.04	0	564.8	795.2	564.8	0
n = 3	t = 0.06	0	457.9	647.7	457.9	0
n = 8	t = 0.16	0	162.2	229.4	162.2	0
n = 9	t = 0.18	0	131.8	186.4	131.8	0
n = 10	t = 0.20	0	107.1	151.4	107.1	0
Exact	t = 0.20	0	125.1	176.9	125.1	0
Error	t = 0.20	0	18	25.4	18	0

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Explicit Results $f = 0.64$

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0.00	x = 0.25	x = 0.50	x = 0.75	x = 1.00
	t = 0	1000	1000	1000	1000	1000
n = 0	t = 0+	0	1000	1000	1000	0
n = 1	t = 0.04	0	360	1000	360	0
n = 2	t = 0.08	0	539.2	180.8	539.2	0
n = 3	t = 0.12	0	-35.3	639.6	-35.3	0
n = 4	t = 0.16	0	419.2	-224.2	419.2	0
n = 5	t = 0.20	0	-260.9	599.3	-260.9	0
Exact	t = 0.20	0	125.1	176.9	125.1	0
Error	t = 0.20	0	385.9	422.5	385.9	0

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What Happened?

- We are seeing effects of instability
- Difference equations may not converge
 - Unstable equations grow without bound
 - May have stable equations that produce incorrect results
 - Conditional stability requires step size less than that needed for accuracy
 - Goal of absolute stability not always possible
 - Discussions of stability complex, can sometimes use physical arguments

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Stability of Explicit Method

- If the values of T_{i+1} and T_{i-1} are fixed an increase in T_i^n should increase T_i^{n+1}
- Numerical: $T_i^{n+1} = f(T_{i+1}^n + T_{i-1}^n) + (1 - 2f)T_i^n$
- If f is greater than 0.5, an increase in T_i^n will cause a decrease in T_i^{n+1}
 - We can avoid this incorrect result by keeping $f = \alpha \Delta t / (\Delta x)^2 \leq 0.5$
 - This imposes a time step limit that may be less than the limit required for accuracy in the solution

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Crank-Nicholson Method

- Seek more accurate time derivative
- Provides implicit method
 - Value of T_i^{n+1} depends on other T^{n+1}
 - More work per step, but can take longer time steps with this method
 - Apply to differential equation at time $n + 1/2$

$$\left. \frac{\partial T}{\partial t} \right|_i^{n+\frac{1}{2}} = \frac{T_i^{n+1} - T_i^n}{\frac{\Delta t}{2}} + O[(\Delta t)^2] = \frac{T_i^{n+1} - T_i^n}{\Delta t} + O[(\Delta t)^2] = \alpha \left. \frac{\partial^2 T}{\partial x^2} \right|_i^{n+\frac{1}{2}}$$

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Crank-Nicholson Equation

- See derivation on slides 52-55
 - Final result shown below
- $$-\frac{f}{2}T_{i-1}^{n+1} + (1+f)T_i^{n+1} - \frac{f}{2}T_{i+1}^{n+1} = \frac{f}{2}[T_{i+1}^n + T_{i-1}^n] + (1-f)T_i^n$$
- $$-fT_{i-1}^{n+1} + 2(1+f)T_i^{n+1} - fT_{i+1}^{n+1} = f[T_{i+1}^n + T_{i-1}^n] + 2(1-f)T_i^n$$
- System of equations easily solved by special application of Gauss elimination called Thomas algorithm (slides 56-58)
- $$-fT_{i-1}^{n+1} + 2(1+f)T_i^{n+1} - fT_{i+1}^{n+1} = R_i^n$$

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Crank Nicholson Results

- Results for $\alpha = 1, L = 1, \Delta x = 0.01, \Delta t = 0.0005, f = \alpha \Delta t / (\Delta x)^2 = 5$

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0	x = .01	x = .02	x = .03	x = .04
	t = 0	1000	1000	1000	1000	1000
n = 0	t = 0+	0	1000	1000	1000	1000
n = 1	t = 0.0005	0	-73.35	423.96	690.85	834.09
n = 2	t = 0.001	0	352.75	305.27	440.73	599.81
n = 3	t = 0.0015	0	25.7	320.81	439.19	533.34
n = 4	t = 0.002	0	203.86	209.57	347.52	473.02
n = 5	t = 0.0025	0	56.79	252.91	334.12	422.43
n = 6	t = 0.003	0	141.46	177.47	298.2	397.48

Crank Nicholson Results II

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0	x = .01	x = .02	x = .03	x = .04
n = 7	t = 0.0035	0	66.73	209.02	279.22	363.26
n = 8	t = 0.004	0	109.4	160.3	263.81	347.29
n = 9	t = 0.0045	0	68.71	179.63	245.68	324.49
n = 10	t = 0.005	0	90.79	148.2	237.92	311.75
n = 11	t = 0.0055	0	67.5	159.07	222.68	296.08
n = 12	t = 0.006	0	78.99	138.51	217.76	285.25
n = 13	t = 0.0065	0	65.08	144.07	205.56	273.92
n = 14	t = 0.007	0	70.94	130.31	201.68	264.62
n = 15	t = 0.0075	0	62.29	132.69	192.04	255.97
n = 16	t = 0.008	0	65.1	123.21	188.58	247.99
n = 17	t = 0.0085	0	59.5	123.75	180.95	241.06

Crank Nicholson Results III

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0	x = .01	x = .02	x = .03	x = .04
n = 18	t = 0.009	0	60.65	117	177.71	234.21
n = 19	t = 0.0095	0	56.86	116.5	171.59	228.43
n = 20	t = 0.01	0	57.1	111.53	168.52	222.53
n = 21	t = 0.0105	0	54.43	110.47	163.53	217.57
n = 22	t = 0.011	0	54.19	106.68	160.64	212.45
n = 23	t = 0.0115	0	52.22	105.35	156.49	208.11
n = 24	t = 0.012	0	51.73	102.36	153.78	203.64
n = 25	t = 0.0125	0	50.21	100.93	150.27	199.78
Exact	t = 0.0125	0	50.43	100.66	150.48	199.72
Error	t = 0.0125	0	0.216	0.272	0.212	0.061

Fully Implicit Method

- Discretize diffusion equation at t_{n+1}

$$\frac{\partial T}{\partial t} \Big|_i^{n+1} = \frac{T_i^{n+1} - T_i^n}{\Delta t} + O(\Delta t) \quad \text{and} \quad \frac{\partial^2 T}{\partial x^2} \Big|_i^{n+1} = \frac{T_{i+1}^{n+1} + T_{i-1}^{n+1} - 2T_i^{n+1}}{(\Delta x)^2} + O[(\Delta x)^2]$$
$$\frac{\partial T}{\partial t} \Big|_i^{n+1} - \alpha \frac{\partial^2 T}{\partial x^2} \Big|_i^{n+1} = \frac{T_i^{n+1} - T_i^n}{\Delta t} - \alpha \frac{T_{i+1}^{n+1} + T_{i-1}^{n+1} - 2T_i^{n+1}}{(\Delta x)^2} + O[(\Delta t), (\Delta x)^2] = 0$$
$$-fT_{i-1}^{n+1} + (1 + 2f)T_i^{n+1} - fT_{i+1}^{n+1} = T_i^n$$

- Tridiagonal system of equations
- Almost same work as CN and no spurious oscillations, but less accuracy

Fully Implicit Results

- Same as CN results: $\alpha = 1, L = 1, \Delta x = 0.01, \Delta t = 0.0005, f = \alpha \Delta t / (\Delta x)^2 = 5$

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0	x = .01	x = .02	x = .03	x = .04
	t = 0	1000	1000	1000	1000	1000
n = 0	t = 0+	0	1000	1000	1000	1000
n = 1	t = 0.0005	0	358.26	588.17	735.71	830.39
n = 2	t = 0.001	0	218.22	408.43	562.69	682.35
n = 3	t = 0.0015	0	166.26	322.13	460.74	578.96
n = 4	t = 0.002	0	139.05	272.65	396.35	507.18
n = 5	t = 0.0025	0	121.84	240.25	352.17	455.26
n = 6	t = 0.003	0	109.75	217.08	319.77	415.99

Fully Implicit Results II

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0	x = .01	x = .02	x = .03	x = .04
n = 7	t = 0.0035	0	100.65	199.49	294.81	385.13
n = 8	t = 0.004	0	93.50	185.57	274.85	360.14
n = 9	t = 0.0045	0	87.68	174.19	258.43	339.38
n = 10	t = 0.005	0	82.82	164.67	244.62	321.81
n = 11	t = 0.0055	0	78.69	156.56	232.81	306.69
n = 12	t = 0.006	0	75.13	149.54	222.55	293.50
n = 13	t = 0.0065	0	72.00	143.38	213.53	281.87
n = 14	t = 0.007	0	69.24	137.93	205.52	271.52
n = 15	t = 0.0075	0	66.77	133.05	198.35	262.22
n = 16	t = 0.008	0	64.55	128.66	191.88	253.82
n = 17	t = 0.0085	0	62.54	124.67	186.01	246.17

Fully Implicit Results III

		i = 0	i = 1	i = 2	i = 3	i = 4
		x = 0	x = .01	x = .02	x = .03	x = .04
n = 18	t = 0.009	0	60.70	121.03	180.64	239.17
n = 19	t = 0.0095	0	59.02	117.70	175.71	232.74
n = 20	t = 0.01	0	57.47	114.62	171.16	226.79
n = 21	t = 0.0105	0	56.03	111.78	166.95	221.28
n = 22	t = 0.011	0	54.70	109.13	163.04	216.16
n = 23	t = 0.0115	0	53.46	106.67	159.38	211.37
n = 24	t = 0.012	0	52.30	104.36	155.96	206.88
n = 25	t = 0.0125	0	51.21	102.20	152.76	202.67
Exact	t = 0.0125	0	50.43	100.66	150.48	199.72
Error	t = 0.0125	0	0.779	1.542	2.273	2.956

Richardson/Leapfrog

- Use two time step central differences

$$\frac{\partial T}{\partial t} \Big|_i = \frac{T_i^{n+1} - T_i^{n-1}}{2\Delta t} + O[(\Delta t)^2] = \alpha \frac{\partial^2 T}{\partial x^2} \Big|_i = \alpha \frac{T_{i+1}^n + T_{i-1}^n - 2T_i^n}{(\Delta x)^2} + O[(\Delta x)^2]$$

- Result is explicit with second order accuracy in time

$$T_i^{n+1} = T_i^{n-1} + \frac{2\alpha\Delta t}{(\Delta x)^2} (T_{i+1}^n + T_{i-1}^n - 2T_i^n) = T_i^{n-1} + 2f(T_{i+1}^n + T_{i-1}^n - 2T_i^n)$$

- However result is unstable for any f and cannot be used

DuFort Frankel

- Modification of Richardson method to provide stability
- Replace $2T_i^n$ in second derivative by average at time steps n+1 and n-1
- Introduces another $O[(\Delta t)^2]$ error

$$\frac{\partial T}{\partial t} \Big|_i = \frac{T_i^{n+1} - T_i^{n-1}}{2\Delta t} + O[(\Delta t)^2] = \alpha \frac{\partial^2 T}{\partial x^2} \Big|_i = \alpha \frac{T_{i+1}^n + T_{i-1}^n - 2T_i^n}{(\Delta x)^2} + O[(\Delta x)^2]$$
$$2T_i^n = T_i^{n+1} + T_i^{n-1} + O[(\Delta t)^2]$$
$$\frac{T_i^{n+1} - T_i^{n-1}}{2\Delta t} = \alpha \frac{T_{i+1}^n + T_{i-1}^n - \frac{T_i^{n+1} + T_i^{n-1}}{2}}{(\Delta x)^2} + O[(\Delta x)^2, (\Delta t)^2, \frac{(\Delta t)^2}{(\Delta x)^2}]$$

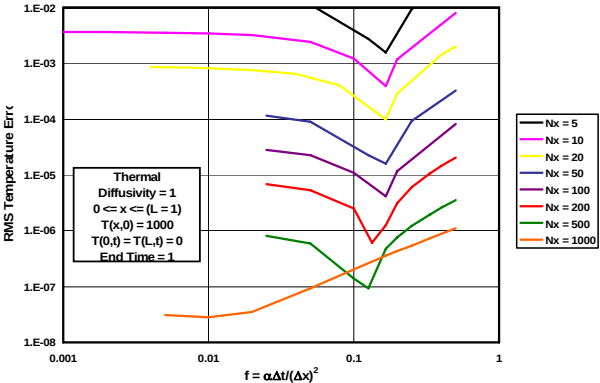
DuFort Frankel

- Rearrange and introduce $f = \alpha\Delta t/(\Delta x)^2$

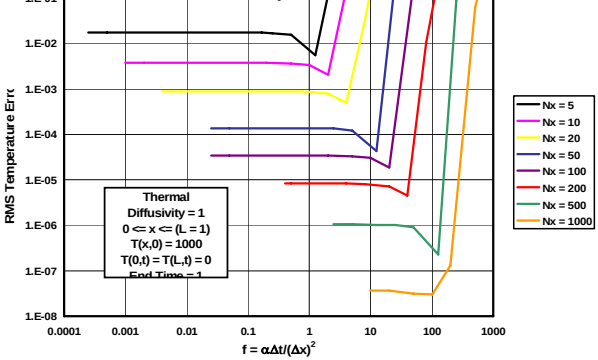
$$T_i^{n+1} - T_i^{n-1} = \frac{2\alpha\Delta t}{(\Delta x)^2} (T_{i+1}^n + T_{i-1}^n - T_i^{n+1} - T_i^{n-1}) = 2f(T_{i+1}^n + T_{i-1}^n - T_i^{n+1} - T_i^{n-1})$$
$$(1 + 2f)T_i^{n+1} = T_i^{n-1}(1 - 2f) + 2f(T_{i+1}^n + T_{i-1}^n)$$

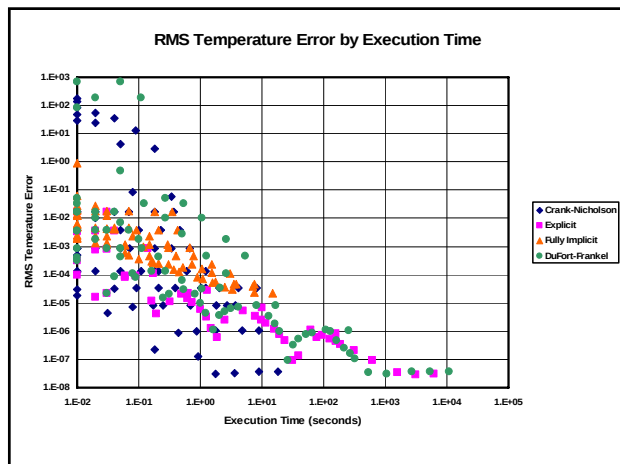
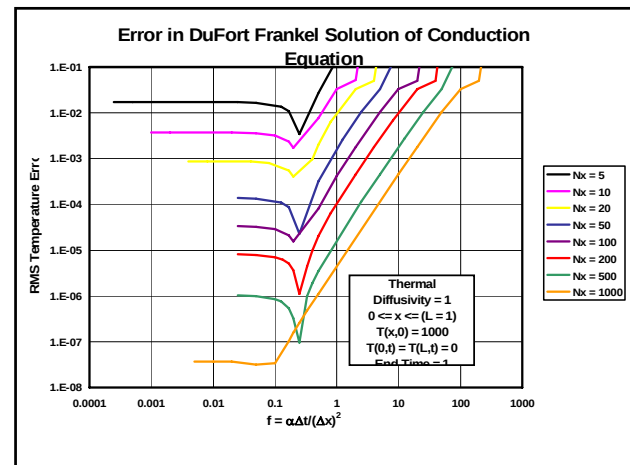
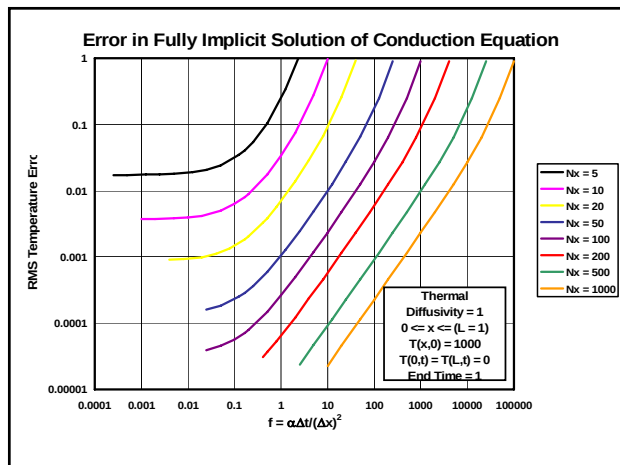
- Result is explicit for values at time n+1
- Explicit start required to get first set of values at time n-1

Error in Explicit Solution of Conduction Equation



Error in Crank-Nicholson Solution of Conduction Equation





Derivation Details

- Slides 53 to 55 cover derivation of Crank-Nicolson method
 - Show how using midpoint of interval for difference equation gives truncation error that is $O[(\Delta x)^2, (\Delta t)^2]$
- Slides 56 to 58 discuss Thomas algorithm
 - Provides efficient numerical solutions for simultaneous equations of following form

$$-fT_{i-1}^{n+1} + 2(1+f)T_i^{n+1} - fT_{i+1}^{n+1} = R_i^n$$

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Space Derivative at $t_{n+1/2}$

- Take average of space derivative at time steps n and $n+1$
- Show average is second order accurate

$$\begin{aligned} f_{i+1} &= f_i + f'_i h + f''_i \frac{h^2}{2} + f'''_i \frac{h^3}{6} + \dots \\ + f_{i-1} &= f_i - f'_i h + f''_i \frac{h^2}{2} - f'''_i \frac{h^3}{6} + \dots \\ \hline f_{i+1} + f_{i-1} &= 2f_i + 2f''_i \frac{h^2}{2} + 2f'''_i \frac{h^4}{24} + \dots \\ f_i &= \frac{f_{i+1} + f_{i-1}}{2} - f''_i \frac{h^2}{4} + f'''_i \frac{h^4}{48} + \dots = \frac{f_{i+1} + f_{i-1}}{2} + O(h^2) \end{aligned}$$

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Using Space Derivative at $t_{n+1/2}$

- Apply average to space derivative

$$\frac{\partial^2 T}{\partial x^2} \Big|_i^{n+1/2} = \frac{1}{2} \left[\frac{\partial^2 T}{\partial x^2} \Big|_i^n + \frac{\partial^2 T}{\partial x^2} \Big|_i^{n+1} \right] + O[(\Delta t)^2]$$

- Substitute into unsteady equation

$$\begin{aligned} \frac{\partial T}{\partial t} \Big|_i^{n+1/2} - \alpha \frac{\partial^2 T}{\partial x^2} \Big|_i^{n+1/2} &= \frac{T_i^{n+1} - T_i^n}{\Delta t} \\ - \frac{\alpha}{2} \left[\frac{T_{i+1}^{n+1} + T_{i-1}^{n+1} - 2T_i^{n+1}}{(\Delta x)^2} + \frac{T_{i+1}^n + T_{i-1}^n - 2T_i^n}{(\Delta x)^2} \right] + O[(\Delta t)^2, (\Delta x)^2] &= 0 \end{aligned}$$

- Introduce $f = \alpha \Delta t / (\Delta x)^2$ and rearrange

$$- \frac{f}{2} T_{i-1}^{n+1} + (1+f) T_i^{n+1} - \frac{f}{2} T_{i+1}^{n+1} = \frac{f}{2} [T_{i+1}^n + T_{i-1}^n] + (1-f) T_i^n$$

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Crank-Nicholson Equations

$$-fT_{i-1}^{n+1} + 2(1+f)T_i^{n+1} - fT_{i+1}^{n+1} = R_i^n = f[T_{i+1}^n + T_{i-1}^n] + 2(1-f)T_i^n$$

- Rewrite equations in matrix form to show tridiagonal structure (boundary values T_0 and T_N specified)

$$\begin{bmatrix} 2(1+f) & -f & 0 & 0 & \cdots & 0 & 0 \\ -f & 2(1+f) & -f & 0 & \cdots & 0 & 0 \\ 0 & -f & 2(1+f) & -f & \cdots & 0 & 0 \\ 0 & 0 & -f & 2(1+f) & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & 0 & \cdots & 2(1+f) & -f \\ 0 & 0 & 0 & 0 & \cdots & -f & 2(1+f) \end{bmatrix} \begin{bmatrix} T_1^{n+1} \\ T_2^{n+1} \\ T_3^{n+1} \\ \vdots \\ T_{N-2}^{n+1} \\ T_{N-1}^{n+1} \end{bmatrix} = \begin{bmatrix} R_1^n + fT_0^n \\ R_2^n \\ R_3^n \\ \vdots \\ R_{N-2}^n \\ R_{N-1}^n + fT_N^n \end{bmatrix}$$

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Thomas Algorithm

- General format for tridiagonal equations

$$\begin{bmatrix} B_0 & C_0 & 0 & 0 & \cdots & 0 & 0 \\ A_1 & B_1 & C_1 & 0 & \cdots & 0 & 0 \\ 0 & A_2 & B_2 & C_2 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & 0 & \cdots & B_{N-1} & C_{N-1} \\ 0 & 0 & 0 & 0 & \cdots & A_N & B_N \end{bmatrix} \begin{bmatrix} x_0 \\ x_1 \\ x_2 \\ \vdots \\ x_{N-1} \\ x_N \end{bmatrix} = \begin{bmatrix} D_0 \\ D_1 \\ D_2 \\ \vdots \\ D_{N-1} \\ D_N \end{bmatrix}$$

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Thomas Algorithm II

- Gauss elimination upper triangular form

$$\begin{bmatrix} 1 & -E_0 & 0 & 0 & \cdots & 0 & 0 \\ 0 & 1 & -E_1 & 0 & \cdots & 0 & 0 \\ 0 & 0 & 1 & -E_2 & \cdots & 0 & 0 \\ 0 & 0 & 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & 0 & \cdots & 1 & -E_{N-1} \\ 0 & 0 & 0 & 0 & \cdots & 0 & 1 \end{bmatrix} \begin{bmatrix} x_0 \\ x_1 \\ x_2 \\ \vdots \\ x_{N-1} \\ x_N \end{bmatrix} = \begin{bmatrix} F_0 \\ F_1 \\ F_2 \\ \vdots \\ F_{N-1} \\ F_N \end{bmatrix}$$

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Thomas Algorithm III

- Forward computations

$$\text{Initial: } E_0 = -C_0 / B_0 \quad F_0 = D_0 / B_0$$

For $i = 1, \dots, N-1$:

$$E_i = \frac{-C_i}{B_i + A_i E_{i-1}} \quad F_i = \frac{D_i - A_i F_{i-1}}{B_i + A_i E_{i-1}}$$

- Get last x value first $x_N = F_N = \frac{D_N - A_N F_{N-1}}{B_N + A_N E_{N-1}}$

- Back substitute: $x_i = F_i + E_i x_{i+1}$

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